

Solution Exercise 05-01: Criticality classes and measures

Solution exercise 1 : Condensation

Thermal potential :

$$\text{Reaction :} \quad \Delta T_{ad} = \frac{Q'_{rx}}{c'_p} = \frac{230 \text{ kJ kg}^{-1}}{1,7 \text{ kJ kg}^{-1} \text{ K}^{-1}} = 135 \text{ K}$$

$$\text{Decomposition :} \quad \Delta T_{ad} = \frac{Q'_{rx}}{c'_p} = \frac{150 \text{ kJ kg}^{-1}}{1,7 \text{ kJ kg}^{-1} \text{ K}^{-1}} = 89 \text{ K}$$

Assuming 100 % accumulation, the la decomposition would be triggered and the overall potential was rated « critical ».

Taking the accumulation into account :

$$MTSR = T_p + X_{ac} \cdot \Delta T_{ad} = 40 + 0,3 \times 135 = 81^\circ \text{C}$$

$MTSR < T_{D24} = 130^\circ \text{C}$, hence the decomposition will not be triggered after a cooling failure, as long as the feed is immediately stopped.

The thermal potential is rated « negligible », but the boiling point can be reached ($MTT = 56^\circ \text{C} = 329 \text{ K}$)

The criticality class is 3.

The amount of vapour released is :

$$M_v = \frac{(MTSR - MTT) \cdot c'_p \cdot M_r}{\Delta H'_v} = \frac{(81^\circ \text{C} - 56^\circ \text{C}) \times 1,7 \text{ kJ kg}^{-1} \text{ K}^{-1} \times 2500 \text{ kg}}{523 \text{ kJ kg}^{-1}} = 203 \text{ kg}_{vap}$$

$$\rho_v = \frac{PM_w}{RT} = \frac{1 \text{ bar} \times 58 \text{ kg kmol}^{-1}}{0,08315 \text{ m}^3 \text{ bar kmol}^{-1} \text{ K}^{-1} \times 329 \text{ K}} = 2,12 \text{ kg m}^{-3}$$

The volume of flammable mixture is :

$$V_{ex} = \frac{M_v}{\rho_v \cdot LIE} = \frac{203 \text{ kg}}{2,12 \text{ kg m}^{-3} \times 0,016} \cong 5885 \text{ m}^3$$

$$\text{Extension : } r = \sqrt[3]{\frac{3V_{ex}}{2\pi}} = \sqrt[3]{\frac{3 \times 5885}{2 \times 3,14}} \approx 14 \text{ m}$$

The flammable cloud may reach the site fences : severity rated « critical ».

Thermal activity at MTT :

$$q_{(MTT)} = q_{rx} \cdot \exp \left[\frac{E}{R} \left(\frac{1}{T_p} - \frac{1}{MTT} \right) \right] \cdot \frac{MTSR - MTT}{MTSR - T_p}$$

$$q_{(MTT)} = 20 \text{ W kg}^{-1} \cdot \exp \left[\frac{100000}{8,314} \left(\frac{1}{313} - \frac{1}{329} \right) \right] \cdot \frac{81 - 56}{81 - 40} = 20 \times 6,5 \times 0,6 \approx 80 \text{ W kg}^{-1}$$

The total heat release is 200kW for the charge of 2500 kg. Hence the condenser power of 250 kW is sufficient.

Vapour velocity :

- Mass flow rate : $\dot{m}_v = \frac{80 \text{ W kg}^{-1} \times 2500 \text{ kg}}{523000 \text{ J kg}^{-1}} = 0,382 \text{ kg s}^{-1}$
- Volume flow rate : $\dot{v}_v = \frac{0,382 \text{ kg s}^{-1}}{2,12 \text{ kg m}^{-3}} = 0,18 \text{ m}^3 \text{ s}^{-1}$
- Pipe section : $S = \pi \frac{0,25^2}{4} = 0,049 \text{ m}^2$
- Vapour velocity : $u = \frac{0,18 \text{ m}^3 \text{ s}^{-1}}{0,049 \text{ m}^2} = 3,7 \text{ m s}^{-1}$

Thus, the probability of loss of control is low. The situation can be mastered as far as the condenser remains in operation in case of cooling failure on the reactor.